

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

<b>Bankfull VELOCITY &amp; DISCHARGE Estimates</b>					
Stream:	Blanchard River		Location:	XS2 (Karg)	
Date:	7/1/2020	Stream Type:	C4	Valley Type:	C-AL-FD
Observers:	J. Ricketts, J. Moyer, N. Uhl		HUC:	4100008	
INPUT VARIABLES			OUTPUT VARIABLES		
Bankfull Riffle Cross-Sectional AREA	790.29	$A_{b\text{kf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	6.18	$d_{b\text{kf}}$ (ft)
Bankfull Riffle WIDTH	127.90	$W_{b\text{kf}}$ (ft)	Wetted PERIMETER $\sim (2 * d_{b\text{kf}}) + W_{b\text{kf}}$	131.68	$W_p$ (ft)
$D_{84}$ at Riffle	103.82	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.34	$D_{84}$ (ft)
Bankfull SLOPE	0.0006	$S_{b\text{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b\text{kf}} / W_p$	6.00	R (ft)
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(\text{ft}) / D_{84}(\text{ft})$	17.60	$R / D_{84}$
Drainage Area	345.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.326	$u^*$ (ft/sec)
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.22	ft / sec	2546.15 cfs
2. Roughness Coefficient: a) Manning's $n$ from Friction Factor / Relative Roughness (Figs. 2-18, 2-19) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.034$			3.39	ft / sec	2675.92 cfs
2. Roughness Coefficient: b) Manning's $n$ from Stream Type (Fig. 2-20) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.019$			6.06	ft / sec	4789.16 cfs
2. Roughness Coefficient: c) Manning's $n$ from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for $n =$ <input type="text"/>			-	ft / sec	- cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Leopold, Wolman and Miller)			3.33	ft / sec	2629.30 cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>			-	ft / sec	- cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$			-	ft / sec	- cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$			3.03	ft / sec	2391.00 cfs
<b>Protrusion Height Options for the <math>D_{84}</math> Term in the Relative Roughness Relation (<math>R/D_{84}</math>) – Estimation Method 1</b>					
Option 1. For <b>sand-bed</b> channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.					
Option 2. For <b>boulder-dominated</b> channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.					
Option 3. For <b>bedrock-dominated</b> channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.					
Option 4. For <b>log-influenced</b> channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.					

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

<b>Bankfull VELOCITY &amp; DISCHARGE Estimates</b>						
Stream:	Blanchard River		Location:	XS4 (Cory St.)		
Date:	7/1/2020	Stream Type:	C4	Valley Type:	C-AL-FD	
Observers:	J. Ricketts, J. Moyer, N. Uhl		HUC:	4100008		
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	737.16	$A_{b\text{kf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	6.00	$d_{b\text{kf}}$ (ft)	
Bankfull Riffle WIDTH	122.93	$W_{b\text{kf}}$ (ft)	Wetted PERIMETER $\sim (2 * d_{b\text{kf}}) + W_{b\text{kf}}$	125.27	$W_p$ (ft)	
$D_{84}$ at Riffle	77.00	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.25	$D_{84}$ (ft)	
Bankfull SLOPE	0.0006	$S_{b\text{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b\text{kf}} / W_p$	5.88	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(\text{ft}) / D_{84}(\text{ft})$	23.24	$R / D_{84}$	
Drainage Area	345.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.323	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			3.41	ft / sec	2515.01	cfs
2. Roughness Coefficient: a) Manning's $n$ from Friction Factor / Relative Roughness (Figs. 2-18, 2-19) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.032"/>			3.55	ft / sec	2617.66	cfs
2. Roughness Coefficient: b) Manning's $n$ from Stream Type (Fig. 2-20) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.019"/>			5.98	ft / sec	4408.22	cfs
2. Roughness Coefficient: c) Manning's $n$ from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for $n =$ <input type="text"/>			-	ft / sec	-	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) Darcy-Weisbach (Hey)			3.58	ft / sec	2636.62	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>			-	ft / sec	-	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $u = Q / A$ $Q =$ <input type="text"/> year			-	ft / sec	-	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$			3.24	ft / sec	2391.00	cfs
<b>Protrusion Height Options for the <math>D_{84}</math> Term in the Relative Roughness Relation (<math>R/D_{84}</math>) – Estimation Method 1</b>						
Option 1. For <b>sand-bed</b> channels: Measure 100 "protrusion heights" of sand dunes from the downstream side of feature to the top of feature. Substitute the $D_{84}$ sand dune protrusion height in ft for the $D_{84}$ term in method 1.						
Option 2. For <b>boulder-dominated</b> channels: Measure 100 "protrusion heights" of boulders on the sides from the bed elevation to the top of the rock on that side. Substitute the $D_{84}$ boulder protrusion height in ft for the $D_{84}$ term in method 1.						
Option 3. For <b>bedrock-dominated</b> channels: Measure 100 "protrusion heights" of rock separations, steps, joints or uplifted surfaces above channel bed elevation. Substitute the $D_{84}$ bedrock protrusion height in ft for the $D_{84}$ term in method 1.						
Option 4. For <b>log-influenced</b> channels: Measure "protrusion heights" proportionate to channel width of log diameters or the height of the log on upstream side if embedded. Substitute the $D_{84}$ protrusion height in ft for the $D_{84}$ term in method 1.						

**Worksheet 2-2.** Computations of velocity and bankfull discharge using various methods (Rosgen, 2006b; Rosgen and Silvey, 2007).

<b>Bankfull VELOCITY &amp; DISCHARGE Estimates</b>						
Stream:	Blanchard River		Location:	XS5 (Centennial Park)		
Date:	7/1/2020	Stream Type:	C4	Valley Type:	C-AL-FD	
Observers:	J. Ricketts, J. Moyer, N. Uhl		HUC:	4100008		
INPUT VARIABLES			OUTPUT VARIABLES			
Bankfull Riffle Cross-Sectional AREA	737.57	$A_{b\text{kf}}$ (ft <sup>2</sup> )	Bankfull Riffle Mean DEPTH	5.44	$d_{b\text{kf}}$ (ft)	
Bankfull Riffle WIDTH	135.54	$W_{b\text{kf}}$ (ft)	Wetted PERIMETER $\sim (2 * d_{b\text{kf}}) + W_{b\text{kf}}$	137.85	$W_p$ (ft)	
$D_{84}$ at Riffle	171.33	Dia. (mm)	$D_{84}$ (mm) / 304.8	0.56	$D_{84}$ (ft)	
Bankfull SLOPE	0.0006	$S_{b\text{kf}}$ (ft / ft)	Hydraulic RADIUS $A_{b\text{kf}} / W_p$	5.35	R (ft)	
Gravitational Acceleration	32.2	g (ft / sec <sup>2</sup> )	Relative Roughness $R(\text{ft}) / D_{84}(\text{ft})$	9.52	$R / D_{84}$	
Drainage Area	274.0	DA (mi <sup>2</sup> )	Shear Velocity $u^* = (gRS)^{1/2}$	0.308	$u^*$ (ft/sec)	
ESTIMATION METHODS			Bankfull VELOCITY		Bankfull DISCHARGE	
1. Friction Factor / Relative Roughness $u = [ 2.83 + 5.66 * \text{Log} \{ R / D_{84} \} ] u^*$			2.58	ft / sec	1900.05	cfs
2. Roughness Coefficient: a) Manning's $n$ from Friction Factor / Relative Roughness (Figs. 2-18, 2-19) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.033"/>			3.23	ft / sec	2383.83	cfs
2. Roughness Coefficient: b) Manning's $n$ from Stream Type (Fig. 2-20) $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n =$ <input type="text" value="0.019"/>			5.61	ft / sec	4139.98	cfs
2. Roughness Coefficient: c) Manning's $n$ from Jarrett (USGS): $u = 1.49 * R^{2/3} * S^{1/2} / n$ $n = 0.39 * S^{0.38} * R^{-0.16}$ Note: This equation is applicable to steep, step/pool, high boundary roughness, cobble- and boulder-dominated stream systems; i.e., for $n =$ <input type="text" value="0.017"/>			6.20	ft / sec	4572.93	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>			-	ft / sec	-	cfs
3. Other Methods (Hey, Darcy-Weisbach, Chezy C, etc.) <input type="text"/>			-	ft / sec	-	cfs
4. Continuity Equations: a) Regional Curves Return Period for Bankfull Discharge $Q =$ <input type="text"/> year $u = Q / A$			-	ft / sec	-	cfs
4. Continuity Equations: b) USGS Gage Data $u = Q / A$			3.24	ft / sec	2391.00	cfs
<b>Protrusion Height Options for the <math>D_{84}</math> Term in the Relative Roughness Relation (<math>R/D_{84}</math>) – Estimation Method 1</b>						
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